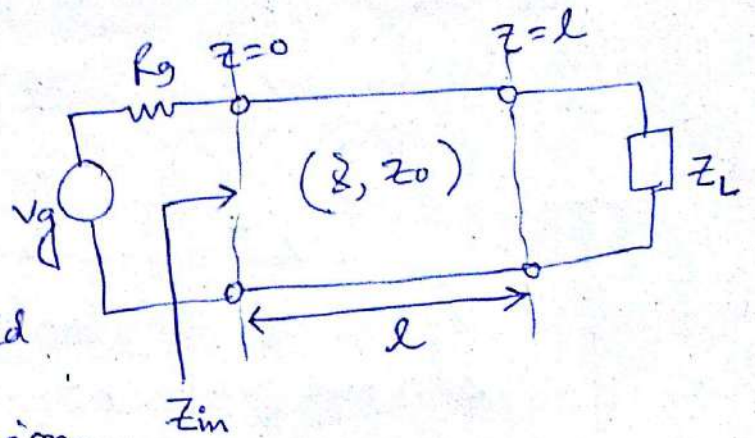


Input Impedance

Input impedance is the line impedance seen at the beginning of the transmission line. The i/p impedance at any point of a transmission line is given by the ratio of the i/p voltage wave to the current wave at that point.

Consider the transmission line of length l , characterized by propagation constant γ and characteristic impedance Z_0 , its connected to the load as shown in figure. Let, the transmission line extend from $z=0$ at generator or sending end to $z=l$ at load end. We have the general voltage and current wave equations in the form of



$$V_s(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z} \quad \dots \text{--- (1)}$$

$$I_s(z) = I_0^+ e^{-\gamma z} + I_0^- e^{+\gamma z} \quad \dots \text{--- (2)}$$

from the definition of characteristic impedance,

$$Z_0 = \frac{V_0^+}{I_0^+} = - \frac{V_0^-}{I_0^-}$$

$$I_0^+ = \frac{V_0^+}{Z_0} \quad \text{and} \quad I_0^- = - \frac{V_0^-}{Z_0}$$

$$\therefore I_s(z) = \frac{1}{Z_0} [V_0^+ e^{-\gamma z} - V_0^- e^{+\gamma z}] \quad \dots \text{--- (3)}$$

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No.

At the sending end, i.e., $z=0$, the voltage and current wave eqⁿs. are reduce to

$$V_s(z=0) = V_s = V_0^+ + V_0^- \quad \dots (4)$$

$$I_s(z=0) = I_s = \frac{1}{Z_0} (V_0^+ - V_0^-) \quad \dots (5)$$

from eqⁿs (4) & (5), we can find out,

$$V_0^+ = \frac{V_s + Z_0 I_s}{2} \quad \dots (6)$$

$$V_0^- = \frac{V_s - Z_0 I_s}{2} \quad \dots (7)$$

So, the voltage and current wave eqⁿs. at any distance z are express as

$$V_s(z) = \frac{V_s + Z_0 I_s}{2} e^{-\gamma z} + \frac{V_s - Z_0 I_s}{2} e^{\gamma z}$$

$$\text{or, } V_s(z) = \frac{1}{2} V_s (e^{\gamma z} + e^{-\gamma z}) - \frac{1}{2} Z_0 I_s (e^{\gamma z} - e^{-\gamma z})$$

$$\text{or, } V_s(z) = V_s \cosh \gamma z - Z_0 I_s \sinh \gamma z \quad \dots (8)$$

Similarly,

$$I_s(z) = \frac{1}{2} I_s (e^{\gamma z} + e^{-\gamma z}) - \frac{1}{2} \frac{V_s}{Z_0} (e^{\gamma z} - e^{-\gamma z})$$

$$\text{or, } I_s(z) = I_s \cosh \gamma z - \frac{V_s}{Z_0} \sinh \gamma z \quad \dots (9)$$

At the receiving end, at $z=l$, the voltage & current wave eqⁿs (8) & (9) can be written as

$$V_s(z=l) = V_L = V_s \cosh \gamma l - Z_0 I_s \sinh \gamma l \quad \dots (10)$$

$$I_s(z=l) = I_L = I_s \cosh \gamma l - \frac{V_s}{Z_0} \sinh \gamma l \quad \dots (11)$$

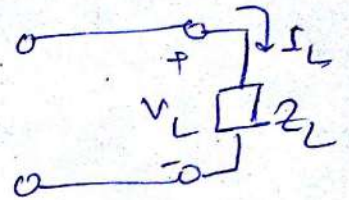
$$\frac{e^{\gamma z} - e^{-\gamma z}}{2} = \sinh \gamma z$$

$$\frac{e^{\gamma z} + e^{-\gamma z}}{2} = \cosh \gamma z$$

When the receiving end of a transmission line is terminated by a load impedance then the voltage across Z_L will be

$$V_L = Z_L I_L \quad \text{--- (12)}$$

Substitute the V_L & I_L in eqⁿ (12),
as



$$V_s \cosh \gamma l - Z_0 I_s \sinh \gamma l = Z_L I_s \cosh \gamma l - \frac{Z_L V_s}{Z_0} \sinh \gamma l$$

or, $V_s \left(\cosh \gamma l + \frac{Z_L}{Z_0} \sinh \gamma l \right) = I_s \left(Z_L \cosh \gamma l + Z_0 \sinh \gamma l \right)$
at the beging of the transmission line,

$$Z_{in} = \frac{V_s}{I_s} = \frac{Z_L \cosh \gamma l + Z_0 \sinh \gamma l}{\cosh \gamma l + \frac{Z_L}{Z_0} \sinh \gamma l}$$

$$= \frac{Z_L + Z_0 \tanh \gamma l}{1 + \frac{Z_L}{Z_0} \tanh \gamma l}$$

$$Z_{in} = Z_0 \cdot \frac{Z_L + Z_0 \tanh \gamma l}{Z_0 + Z_L \tanh \gamma l} \quad \text{--- (13)}$$

This is the i/p impedance for finite lossy transmission line.

For lossless transmission line,

$$\gamma = \alpha + j\beta, \text{ where, } \alpha = 0$$

$$\text{i.e., } \gamma = j\beta$$

$$\text{Hence, } \tan(j\beta l) = j \tan \beta l.$$

then,

$$Z_{in} = Z_0 \cdot \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l}$$

I/p impedance for lossless transmission line.

① Reflection coefficient



Reflection coefficient of a transmission line is the ratio of the reflected voltage (or current) to the incident voltage (or current), when a transmission line is terminated in an impedance Z_L not equal to the characteristic impedance (Z_0) of the line.

The general transmission-line eqⁿ for voltage & current as a function of position along the line are,

$$V_s(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z} \quad \dots \text{--- (1)}$$

$$\text{and } I_s(z) = \frac{1}{Z_0} (V_0^+ e^{-\gamma z} - V_0^- e^{+\gamma z}) \quad \dots \text{--- (2)}$$

The voltage and current at the load ($z=l$) are given as

$$V_s(z=l) = V_L = V_0^+ e^{-\gamma l} + V_0^- e^{+\gamma l} \quad \dots \text{--- (3)}$$

$$\text{and } I_s(z=l) = I_L = \frac{1}{Z_0} (V_0^+ e^{-\gamma l} - V_0^- e^{+\gamma l}) \quad \dots \text{--- (4)}$$

Solving these two eq^s, we get the voltage coefficient in terms of the load voltage and load current as follows

$$V_0^+ = \left(\frac{V_L + Z_0 I_L}{2} \right) e^{\gamma l} \quad \dots \text{--- (5)}$$

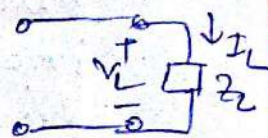
$$V_0^- = \left(\frac{V_L - Z_0 I_L}{2} \right) e^{-\gamma l} \quad \dots \text{--- (6)}$$

The voltage reflection coefficient as a function of position along the line $[\Gamma(z)]$ is defined as the ratio of the reflected voltage wave to the transmitted voltage wave.

$$\Gamma(z) = \frac{V_0^- e^{+\gamma z}}{V_0^+ e^{-\gamma z}} = \frac{V_0^-}{V_0^+} e^{+2\gamma z} \quad \dots \text{--- (7)}$$

Inserting the expressions for the voltage coefficients in term of the load voltage and current, we have,

$$\Gamma(z) = \frac{\left(\frac{V_L - Z_0 I_L}{2}\right) e^{-\gamma l}}{\left(\frac{V_L + Z_0 I_L}{2}\right) e^{+\gamma l}} \cdot e^{2\gamma z}$$



$$= \frac{Z_L - Z_0}{Z_L + Z_0} e^{-2\gamma l} \cdot e^{2\gamma z}$$

$$\therefore \Gamma(z) = \frac{Z_L - Z_0}{Z_L + Z_0} e^{2\gamma(z-l)}$$

The reflection coefficient at the load ($z=l$) is

$$\Gamma(z=l) = \Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Hence, the reflection coefficient as a function of position can be written as,

$$\Gamma(z) = \frac{Z_L - Z_0}{Z_L + Z_0} e^{2\gamma(z-l)} = \Gamma_L e^{2\gamma(z-l)}$$

Note
 $\Rightarrow$

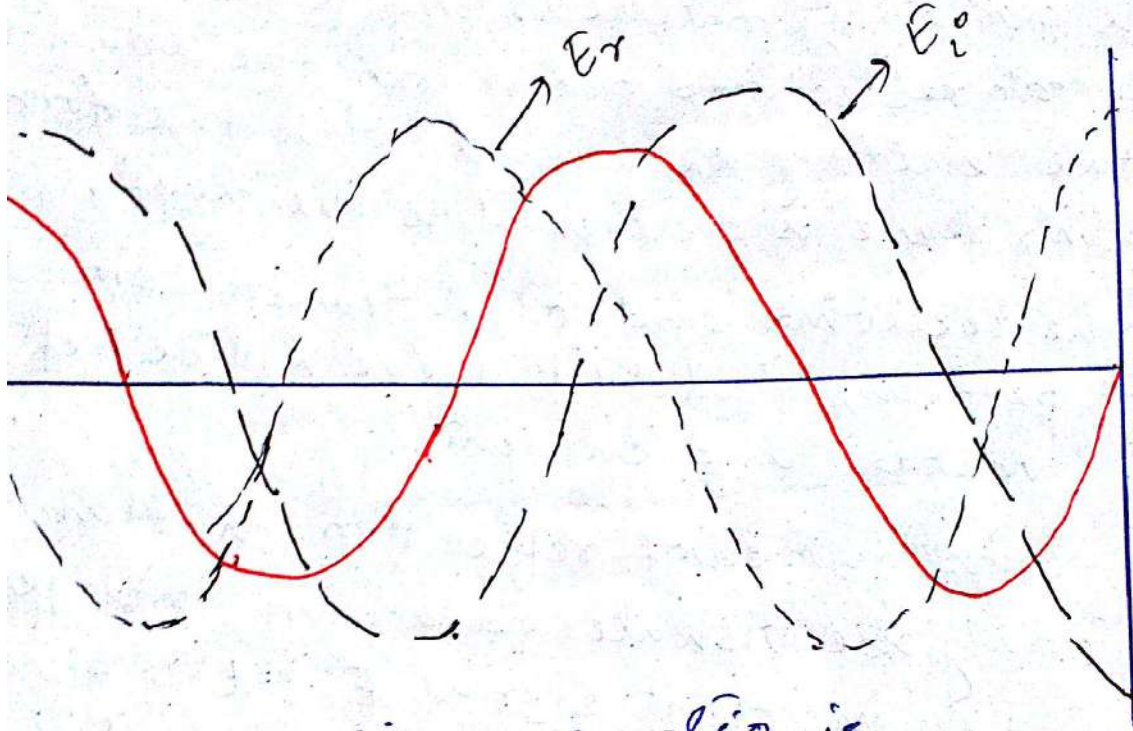
The current reflection coefficient at any point on the line is the negative of the voltage reflection coefficient at that point.



① VSWR (voltage standing Wave Ratio)

- Generally, if $Z_L = Z_0$, then reflection coefficient, $\Gamma_L = 0$, that means, the transmission line is perfectly matched. This is the ideal case where no reflections occur from the load and all the energy associated with the forward-travelling wave is delivered to the load.
- If the receiving end of a transmission line is not perfectly matched, there will be reflection of the voltage and current.
- As a consequence of reflection, a standing wave may be visualised as an interference between the incident signal E_i at a given frequency, travelling in the forward direction, and the reflected signal E_r , at the same frequency, travelling in the reverse direction.
- At the load, the relationship between the amplitudes of E_r and E_i and the phase angle between them are uniquely determined by the load impedance.
- The phase angle between E_r and E_i , however, will vary along the line as a function of the distance from the load.
- Since the wave oscillates in amplitude but never moves laterally, it is called a standing wave.

→ In fig, the incident, reflected and the standing waves can be seen. The dashed lines are the E_r and E_i , while the nondashed one represents the standing wave.



→ The standing wave ratio is defined as the ratio of the maximum voltage (or current) to the minimum voltage (or current) of a line having standing waves

$$S = \frac{V_{\max}}{V_{\min}} = \frac{I_{\max}}{I_{\min}} = \frac{1 + |\Gamma_L|}{1 - |\Gamma_L|}$$

① Establish the relationship between

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$



⇒ We have for a lossless line, the voltage and current given as,

$$V_s(z) = V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z} \quad [\because \alpha = 0]$$

$$I_s(z) = \frac{1}{Z_0} (V_0^+ e^{-j\beta z} - V_0^- e^{+j\beta z})$$

If we let x be the distance from the receiving end, the above two equations can be expressed in terms of x simply by putting $z = -x$.

$$V_s(z=x) = V_0^+ e^{j\beta x} + V_0^- e^{-j\beta x}$$

$$I_s(x) = \frac{1}{Z_0} (V_0^+ e^{j\beta x} - V_0^- e^{-j\beta x})$$

Now, reflection coefficient is given as,

$$\Gamma = |\Gamma| e^{j\theta} = \frac{V_0^- e^{-j\beta x}}{V_0^+ e^{+j\beta x}} = \left(\frac{V_0^-}{V_0^+} \right) e^{-2j\beta x}$$

At receiving end, $x=0$ and θ

$$\Gamma = \Gamma_r = |\Gamma| e^{j\theta} = \left(\frac{V_0^-}{V_0^+} \right)$$

$$V_0^- = V_0^+ |\Gamma| e^{j\theta}$$

Replacing this value, we get,

$$V_s(x) = V_0^+ e^{j\beta x} + V_0^+ |\Gamma| e^{j\theta} e^{-j\beta x}$$

$$\begin{aligned}
 V_s(x) &= V_0 + \left[e^{j\beta x} + |r| e^{j0} e^{-j\beta x} \right] \\
 &= V_0 + e^{j\beta x} \left[1 + |r| e^{j0} e^{-2j\beta x} \right] \\
 &= V_0 + e^{j\beta x} \left[1 + |r| e^{-j(2\beta x - 0)} \right]
 \end{aligned}$$

For the voltage to be maximum, two components must be in phase, so, that-

$$(2\beta x_{\max} - 0) = 2n\pi$$

where, $n = 0, 1, 2, 3, \dots$

The first voltage maximum nearest to the load end will occur when $n = 0$, i.e., $2\beta x_{\max} = 0$.

The magnitude of the maximum voltage is given as,

$$V_{s\max} = V_0 + [1 + |r|]$$

For the voltage to be minimum, two components must be in phase opposition, so that,

$$(2\beta x_{\min} - 0) = (2n+1)\pi$$

where $n = 0, 1, 2, 3, \dots$

The first voltage minimum nearest to the load end will occur when $n = 0$, i.e.,

$$(2\beta x_{\min} - 0) = \pi$$

The magnitude of the minimum voltage is given as,

$$V_{s\min} = V_0 + [1 - |r|]$$

If we take the ratio of maximum and minimum voltages, we get,

$$\boxed{\frac{V_{smax}}{V_{smin}} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = VSWR(S)}$$

##

$$\Gamma = \frac{V_0^- e^{j\beta l}}{V_0^+ e^{-j\beta l}} = \frac{V_r}{V_i} \quad \left| \begin{array}{l} V_r \rightarrow \text{reflected wave} \\ V_i = \text{incident wave} \end{array} \right.$$

$$= \frac{Z_L - Z_0}{Z_L + Z_0}$$

The general form of wave eqⁿ.

$$V_s(z) = V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z}$$

at load, ($z=l$)

$$V_s(z=l) = V_0^+ e^{-j\beta l} + V_0^- e^{+j\beta l}$$

magnitude of $= V_i + V_r$.

The voltage wave is maximum, when V_i & V_r are in same phase.

$$|V_{max}| = |V_i| + |V_r|$$

The magnitude of voltage wave is minimum, when V_i & V_r are in opposite phase,

$$|V_{min}| = |V_i| - |V_r|$$

now,

$$VSWR(S) = \frac{|V_{max}|}{|V_{min}|} = \frac{|V_i| + |V_r|}{|V_i| - |V_r|}$$

$$S = \frac{1 + \left| \frac{V_r}{V_i} \right|}{1 - \left| \frac{V_r}{V_i} \right|} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$